



Semiconductor Power Electronics Technology

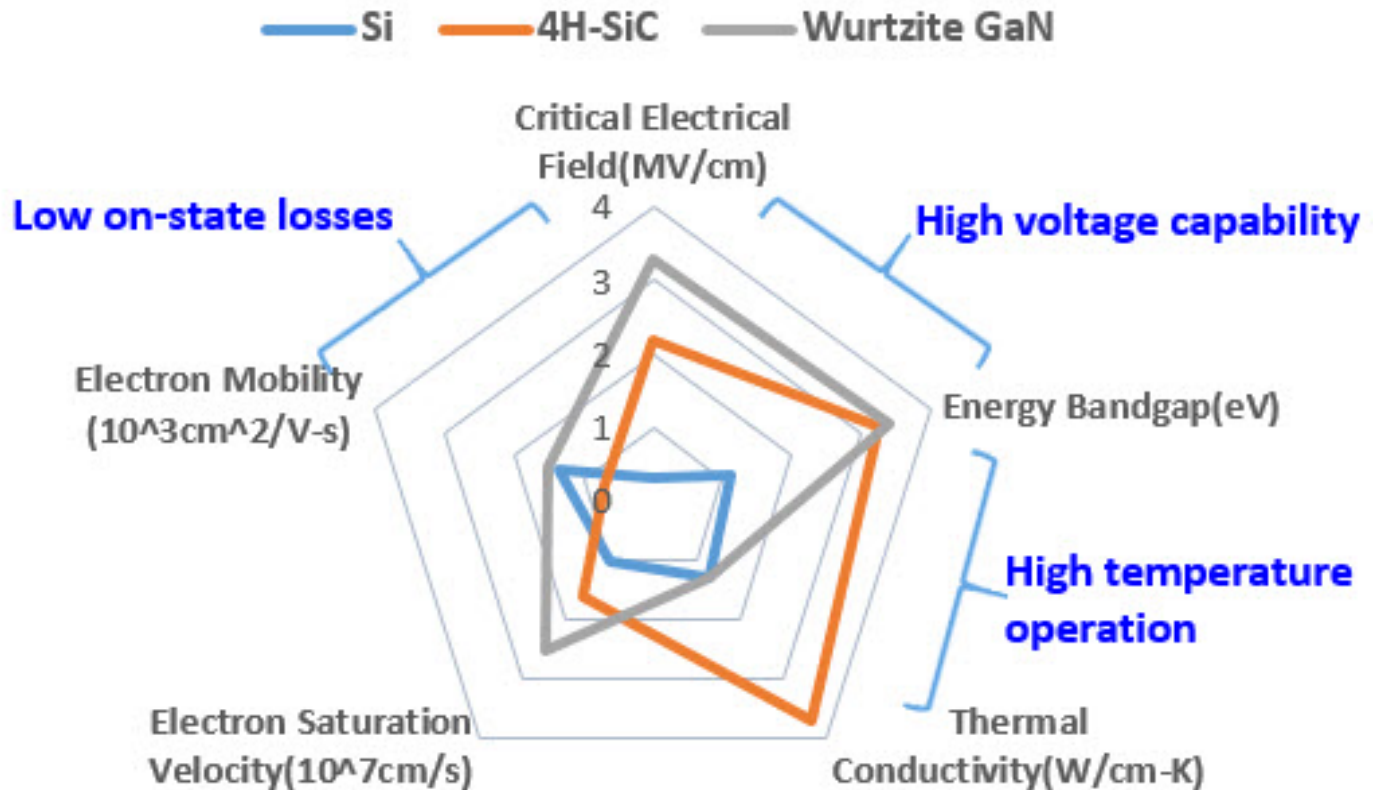
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Nov. 14, 2017

CEM Industry Advisory Panel Meeting

WBG Material Advantages

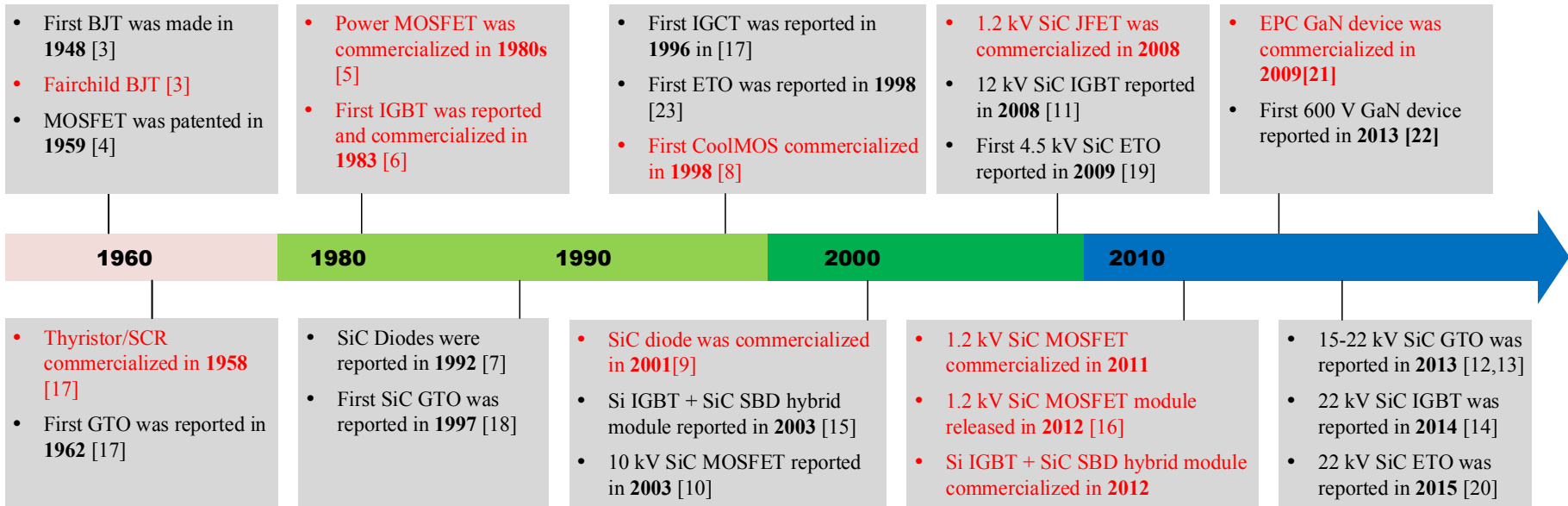


Data source: www.ioffe.ru/SVA/NSM/Semicond/

There are other WBG materials being actively researched, including AlN, GaO, Diamond

Power Semiconductor Milestones

Decades of innovations



Device concepts are more or less settled on several well established concepts

thyristor (symmetric and asymmetric, forced turn-off or line commutated)

IGBT

MOSFET (or other FET variations)

Schottky diode

PN junction diode

Next major trend: move from Si to WBG

1st wave: Si MOSFET/IGBT

2nd superjunction device

3rd moving to WBG: MOSFET as the dominant device concept

Power Device and Me

(1979-1983)



Power MOSFET

(1983-1986)



IGBT

(1989-1992)



Power integrated circuits

(1994-2004)



SiC/IPEM/PEBB

(2004-2017)



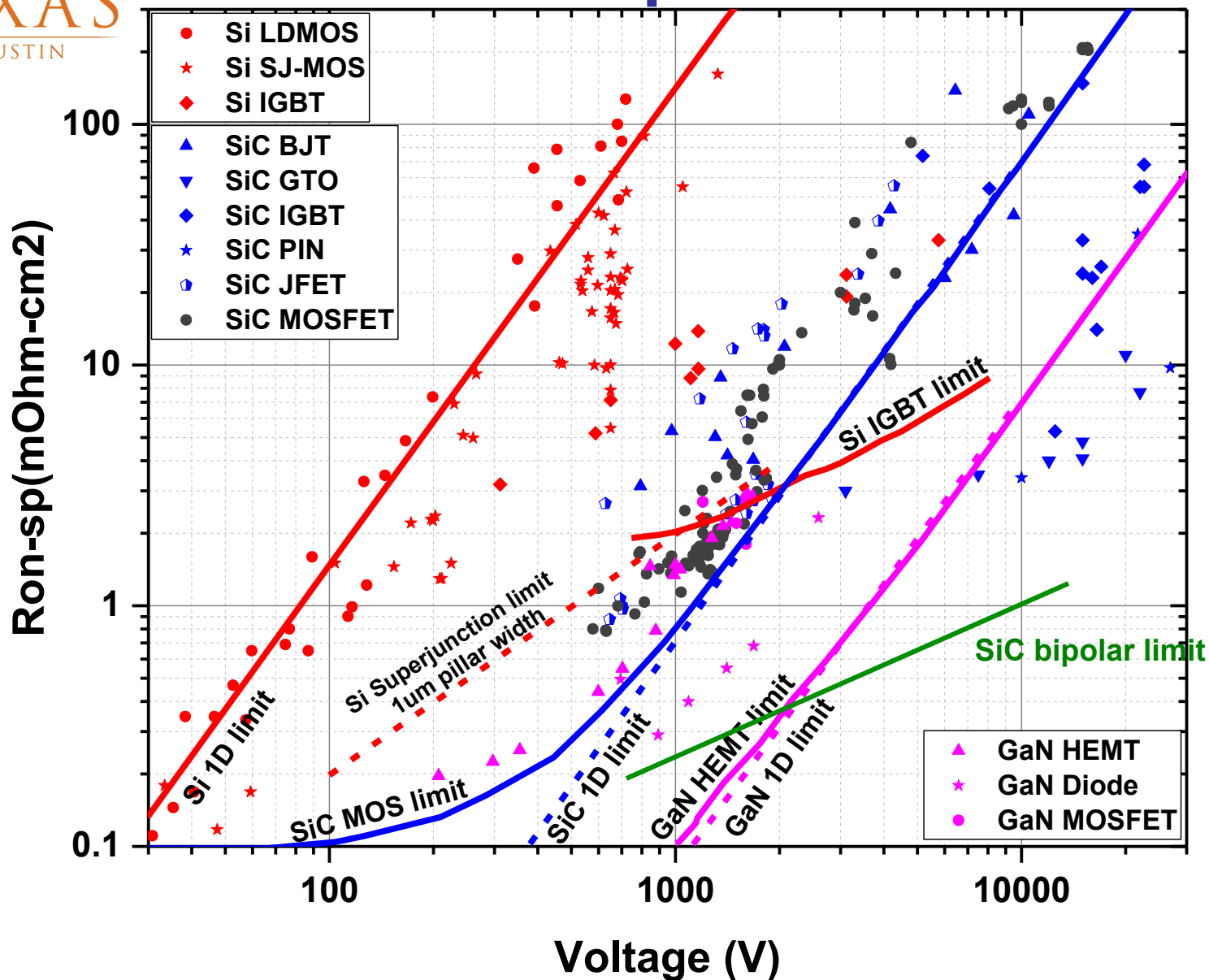
WBG in the grid



WBG cost reduction

- **Power Management IC (PMIC)**
 - Power system on chip design; High voltage integrated circuit; GaN HVIC
- **Power Semiconductor Devices (PSD)**
 - Si, GaN, SiC, GaO power devices
 - Power electronics packaging
- **High Density Power Electronics (HDPE)**
 - GaN/SiC High density power electronics; Driving, thermal and packaging techniques
 - Magnetic materials and devices
- **High Power Electronics (HPE)**
 - High power electronics based on Si solution (IGBT, ETO)
 - Ultra high voltage SiC power electronics
 - Solid State Transformer; Solid State Circuit Breaker, Hybrid breaker
- **Renewable Energy System, Microgrid and Smart Grid (RMS)**
 - Solar/Wind/EV Systems/Wireless Power Transfer/Storage Systems
 - 380V DC Microgrid; Medium Voltage DC (MVDC); High Voltage DC (HVDC)
- **Energy Internet (EI)**
 - Blockchain/Communication/Energy router

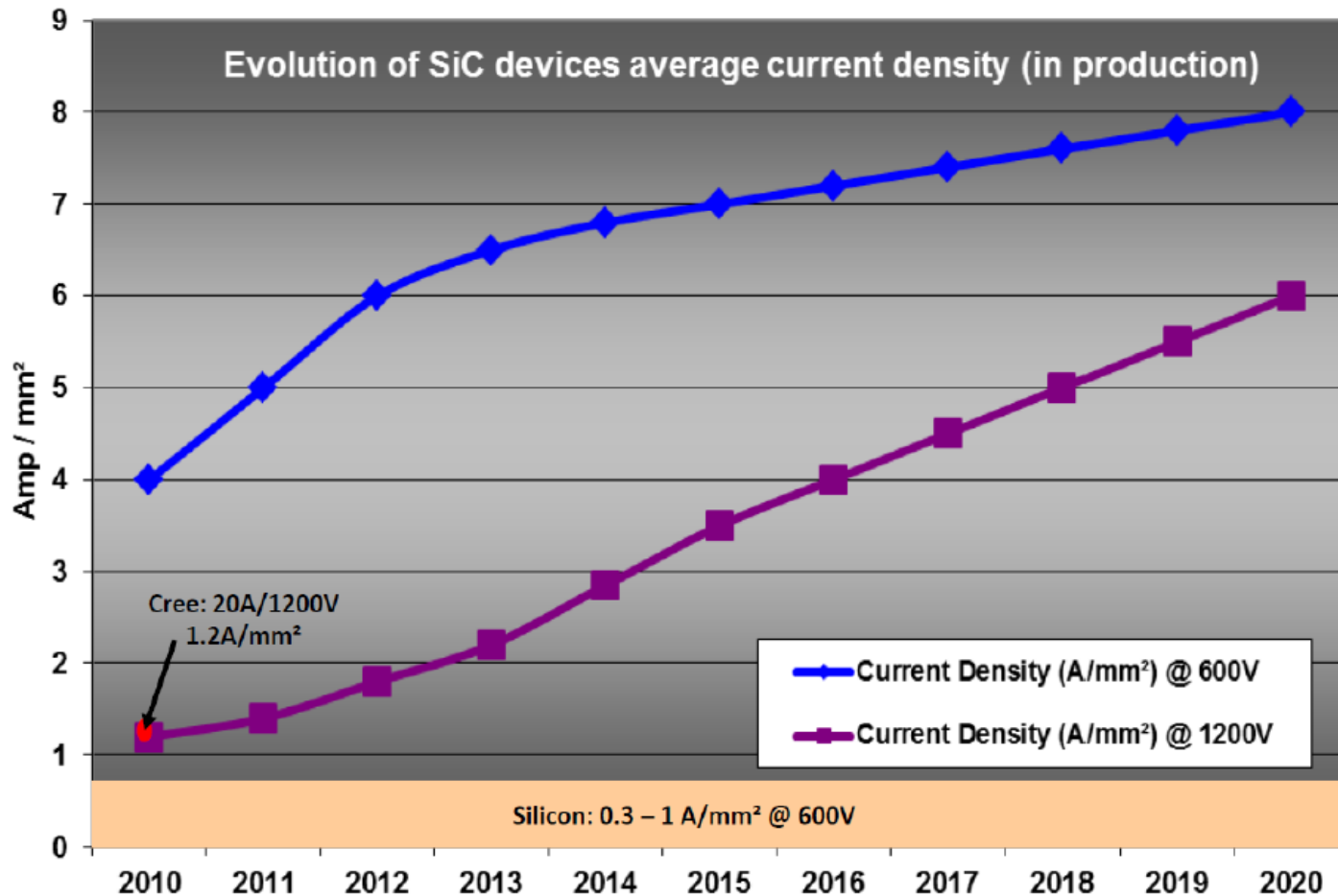
Ron FOM Competition: Current Status



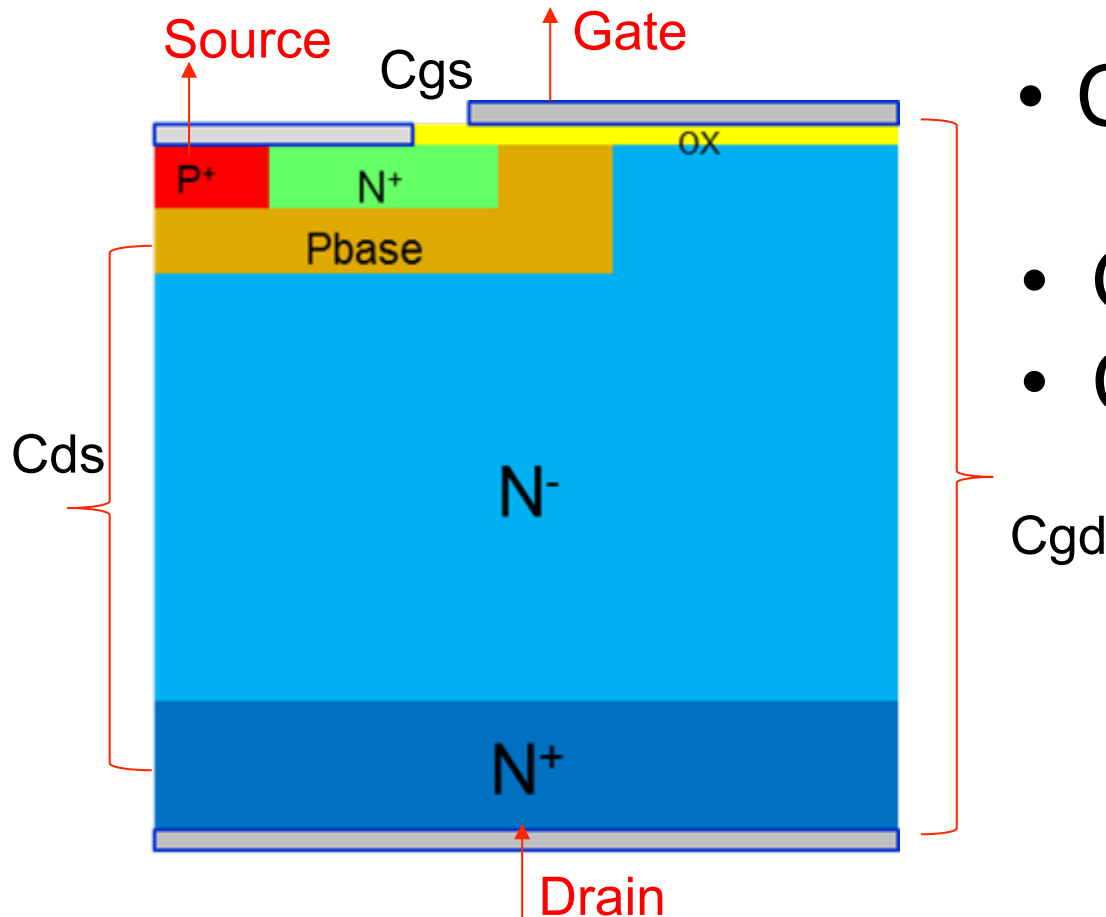
SiC MOSFET: Achieved 100X reduction over Si and 10X over Si SJ
Not much improvement over Si IGBT

Direct Impact: Current Density Increase & Chip Size Reduction

$$J = \sqrt{\frac{VT}{R_{jc-sp} * R_{on-sp}}}$$



Si/SiC: Vertical Power Devices

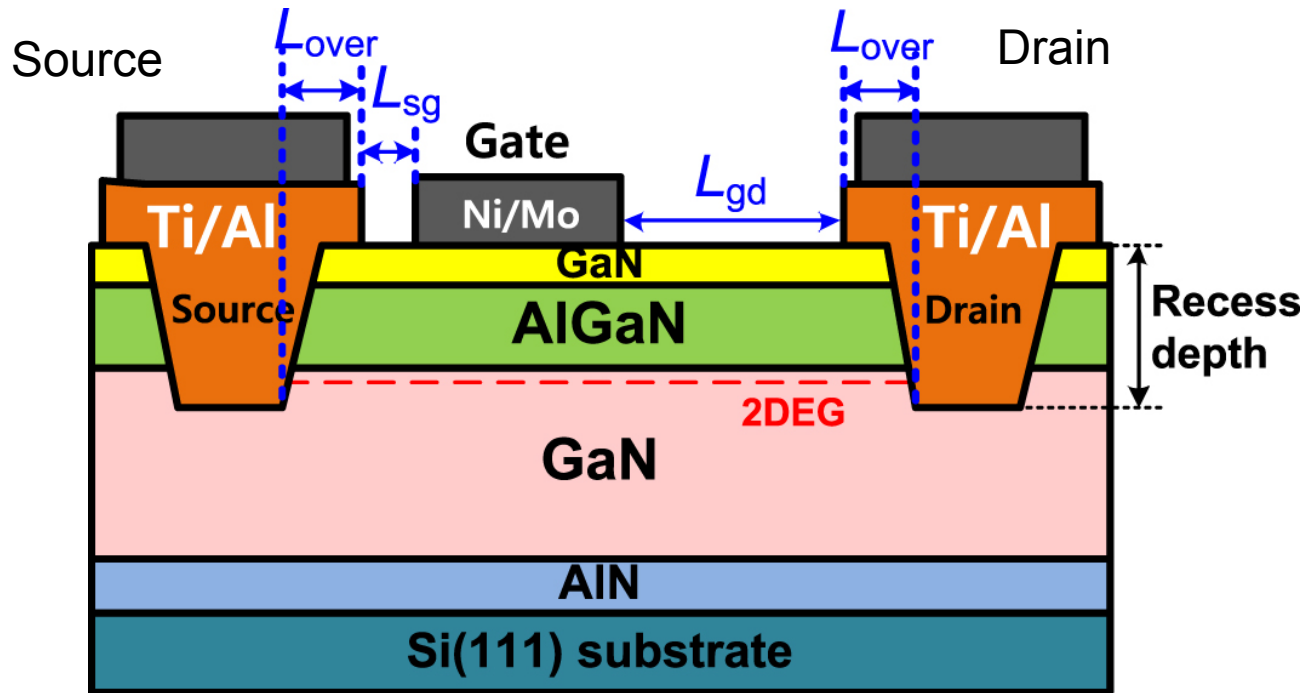


- $C_{gs} \sim C_{ox} \cdot A_{chip}$
- $Q_{oss} \sim \epsilon \cdot E_c \cdot A_{chip}$
- $C_{oss} \sim E_c$

$$dV / dt = \frac{J}{C_{sp}}$$

Since capacitance also increased by 10X
so dV/dt will be similar unless $J(WBG) > 10X J(Si)$

GaN: Lateral Device Construction



Bottomline:

- On Ron, not as good as vertical SiC, still much better than Si
- But even lower capacitance due to the lateral structure!
 C not simply scale with Achip

A Closer Look at Ron, Capacitance, Qrr

600V Devices Compared

600V FETs	Ron (mohm)	Ciss (nF)	FOM 1 (Ron*Ciss)	Coss (nF)@400V	FOM2 (Ron*Coss)	Qrr(uC)	FOM3 (Ron*Qrr)
Si SJ	37	7.24	267	0.38	14	36	1332
SiC MOS	120	1.2	144	0.09	10.8	0.053	6.3
GaN HFET	25	.52	13	0.13	3.25	0.113	2.8

Si SJ: Infineon IPW65R037C6. SiC MOSFET: Rohm SCT2120AF GaN HFET: GaNSystem GS66516T

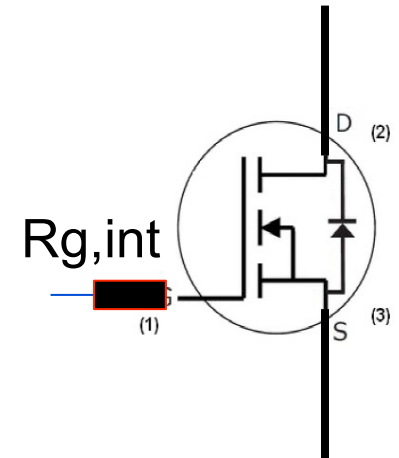
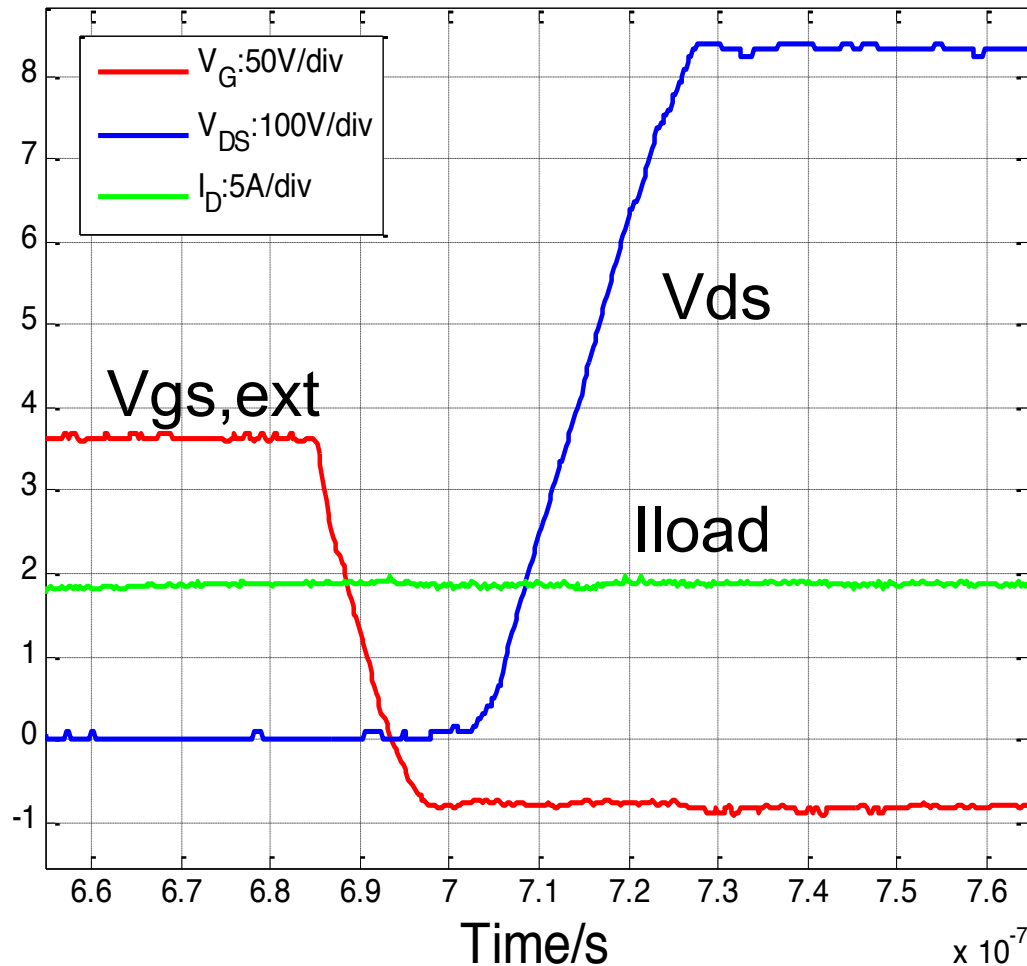
• Gate loop is getting faster & faster

Drain loop
dV/dt increase?
dV/dt ~ I/C = J/C_{sp}

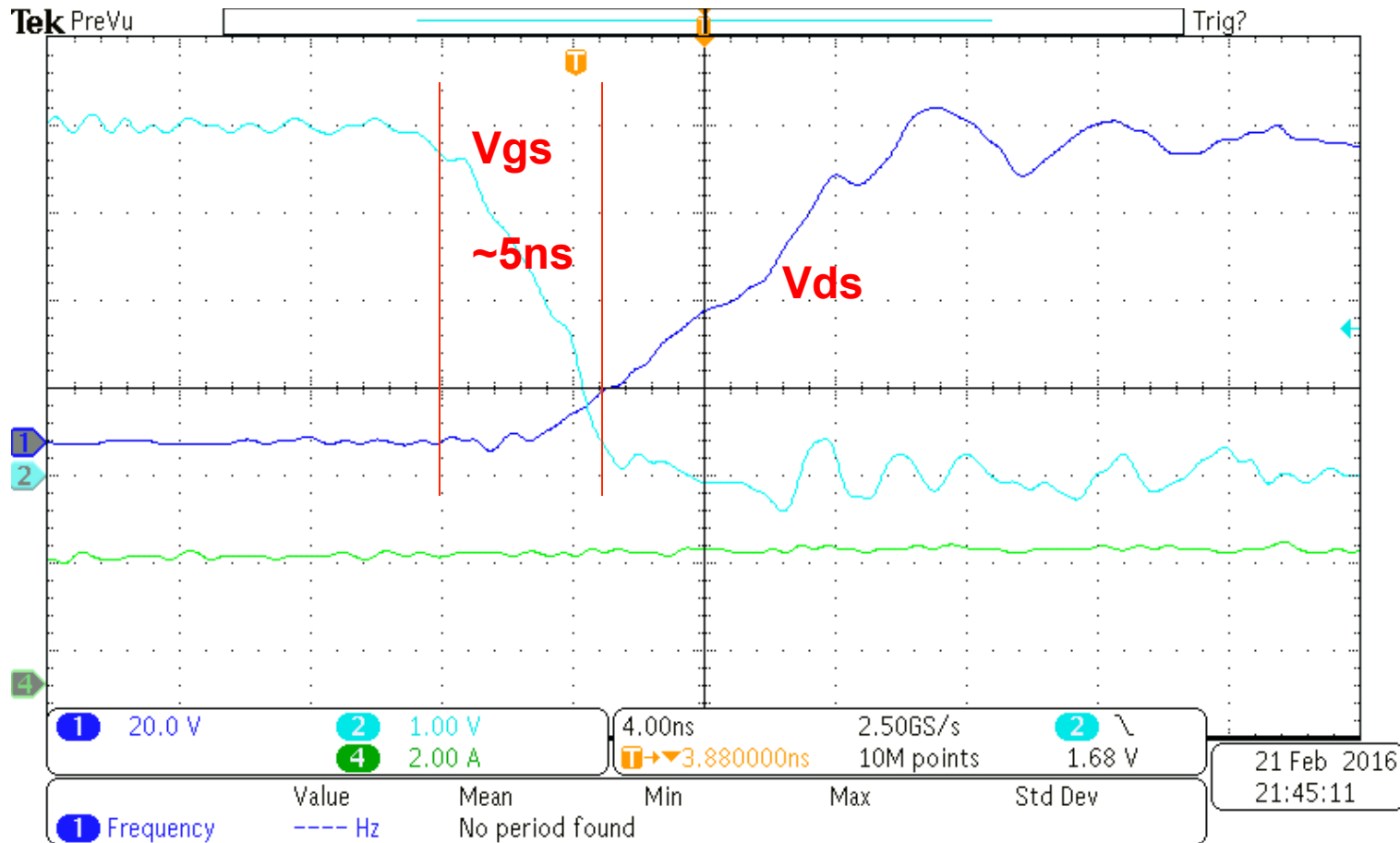
Reverse recovery charge/loss
Basically eliminated in WBG devices

Zero Turn-off Loss (Hard Driven MOSFET)

80 mohm 1200VC SiC MOSFET, $R_{g,ext}=0$, $V=800V$, $I=10A$



650V GaN turn-off waveform



Zero turn-off loss is also achieved in hard-driven GaN

Achieving Zero Switching Loss

➤ Hard switching application

$$E_{on} = E_{on}(\text{measured}) + E_{oss} + E_{oss}(\text{diode} + \text{load cap})$$

$$E_{off} = E_{off}(\text{measured}) - E_{oss} \sim 0 \text{ within ZTL region}$$

$$E_{total} = E_{on} + E_{off} = E_{on}(\text{measured}) + E_{off}(\text{measured})$$

$$\text{Gate drive loss} \sim f_s \cdot V_g \cdot Q_g$$

➤ ZVS soft switching application

$$E_{on} \sim 0$$

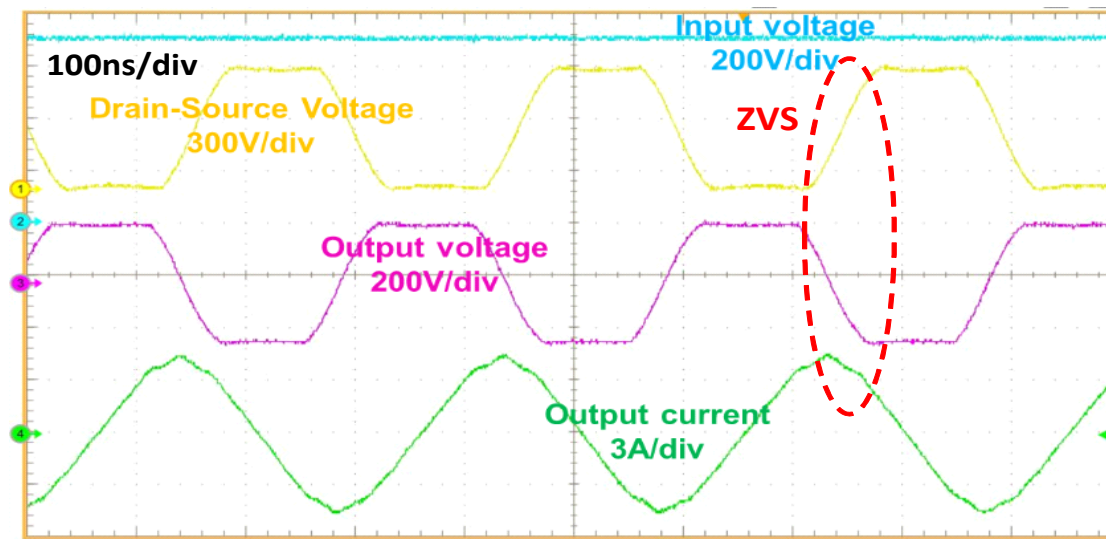
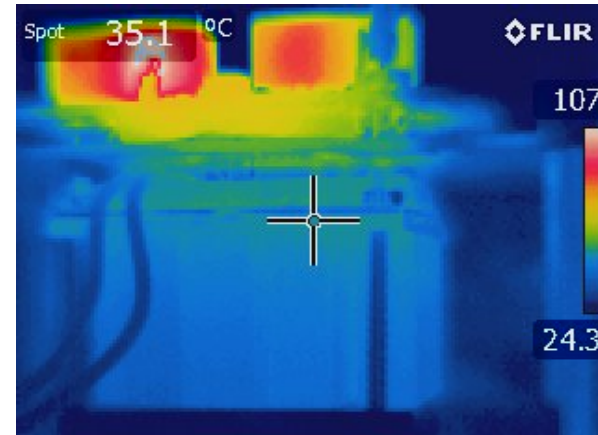
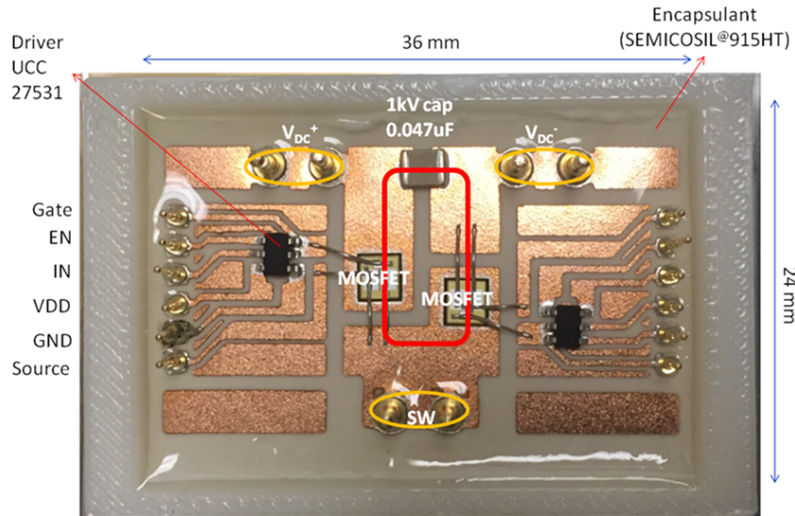
$$E_{off} = E_{off}(\text{measured}) - E_{oss} \sim 0 \text{ within ZTL region}$$

$$E_{total} = E_{on} + E_{off} = 0$$

$$\text{Gate drive loss} \sim f_s \cdot V_g \cdot Q_g$$

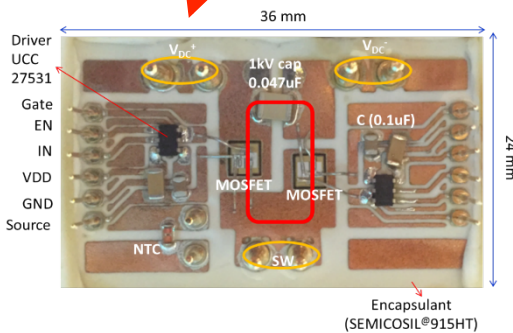
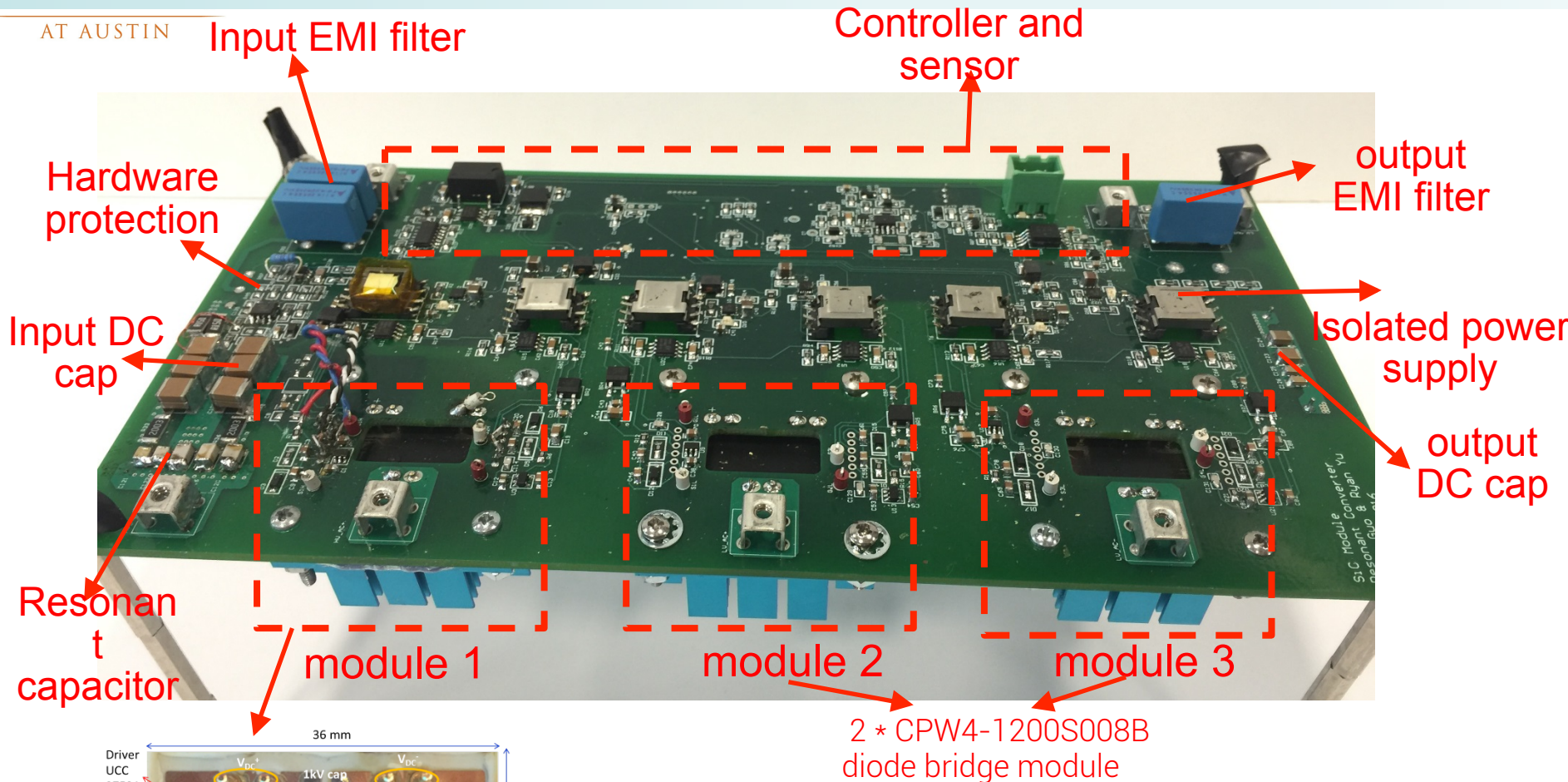
- **Switching frequency no longer a constraint**
- **Ron keeps going down so RMS current less a concern**

3.38 MHz operation of 1200V SiC MOSFET (with ZVS turn-on)



Demonstrated zero switching loss

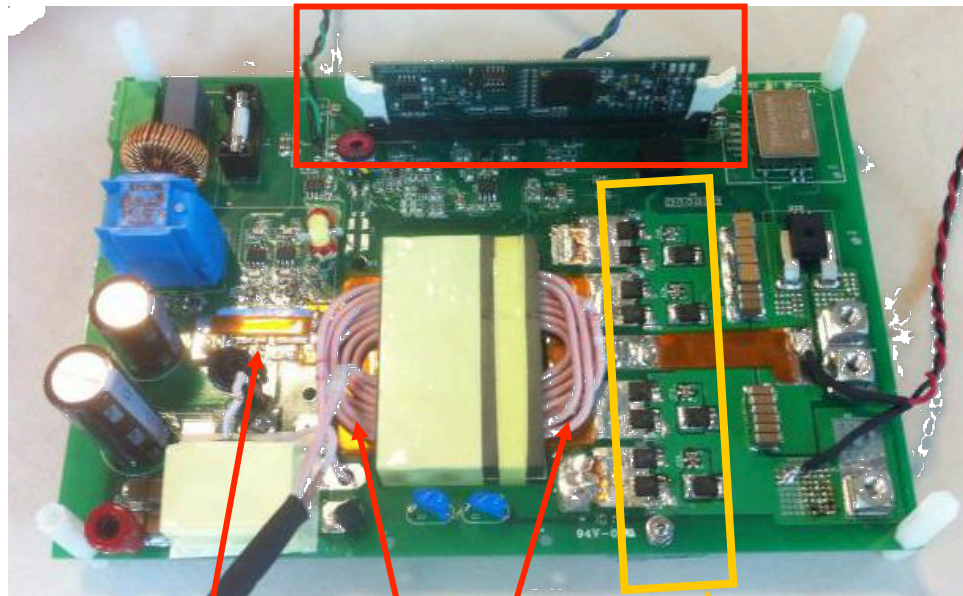
1 MHz LLC Resonant Converter Prototype



Input voltage V_{in}	800 V
Output voltage V_{out}	400 V
Rated Power P_r	4.5 kW
Transformer turns ratio	1 : 1
Leakage inductance, L_{lk}	2 μ H
Magnetizing inductance, L_m	11 μ H
Switching frequency f_{sw}	1.2 MHz

1kW Isolated Bidirectional DC/DC

Controller board



HV GaN device

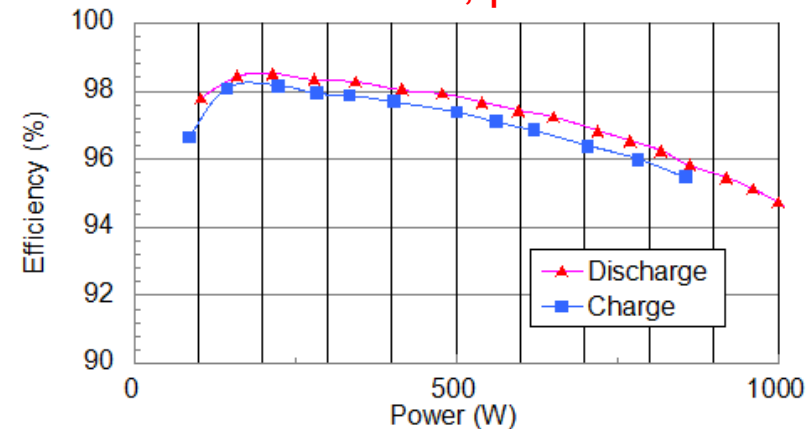
Primary

LV Si device

Picture with 1 kWh battery



400V to 12 V , peak > 98%



Storage capacity

1 kWh

Charge/discharge power

1 kW

LV side voltage (V_{LV})

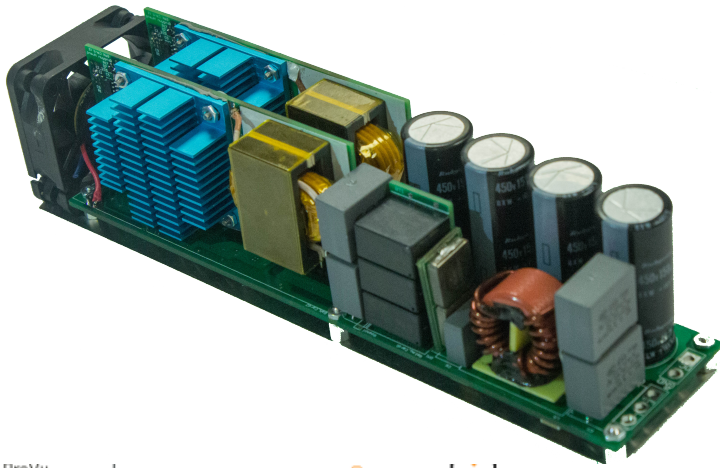
(10.8~14.4)V

HV side voltage (V_{HV})

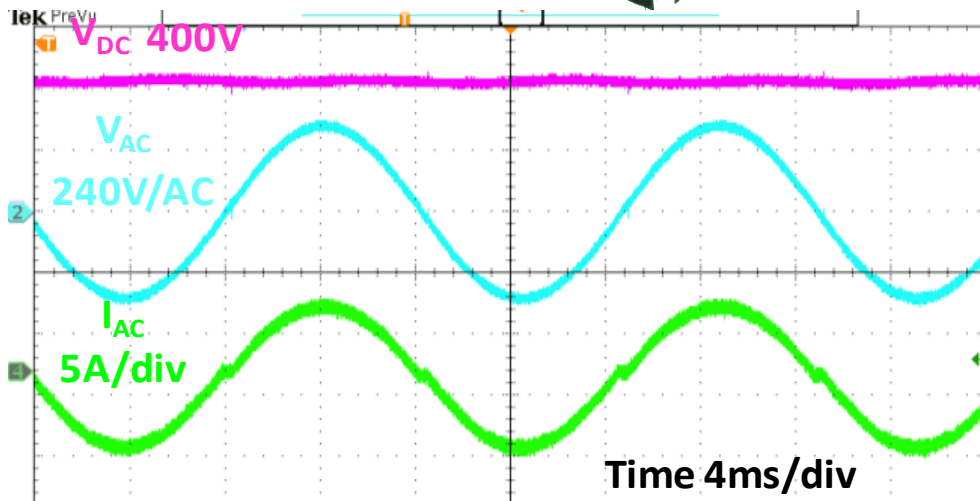
(350~410)V

Project Highlight 3: 3.2kW AC/DC PFC

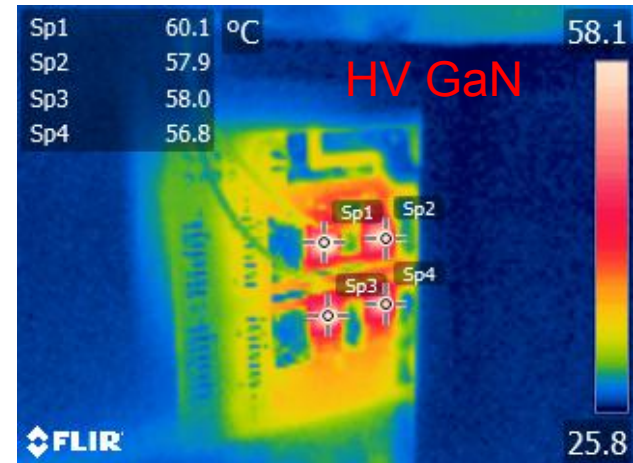
- Two Phase Totem-Pole true bridgeless PFC with full ZVS operation
- HV 650V GaN daughter-boards
- Extreme power density
- Excellent thermal design



Power	3.2 kW
Topology	Two phase Totem-Pole PFC (300k-2 Mhz)
Input	Universal input AC
HV side voltage (V_{HV})	400V
Tested efficiency	>99%
Power density	130 W/inch ³

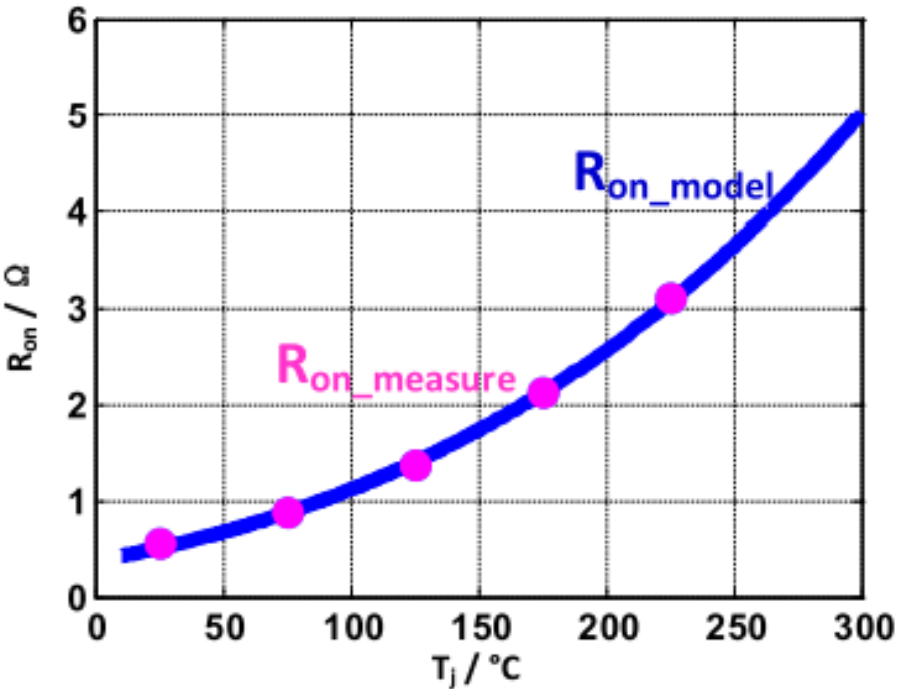


One phase test result at 1.6kW



Only 35°C rise at full power

15 kV SiC MOSFET: 10-20X Increase in BV

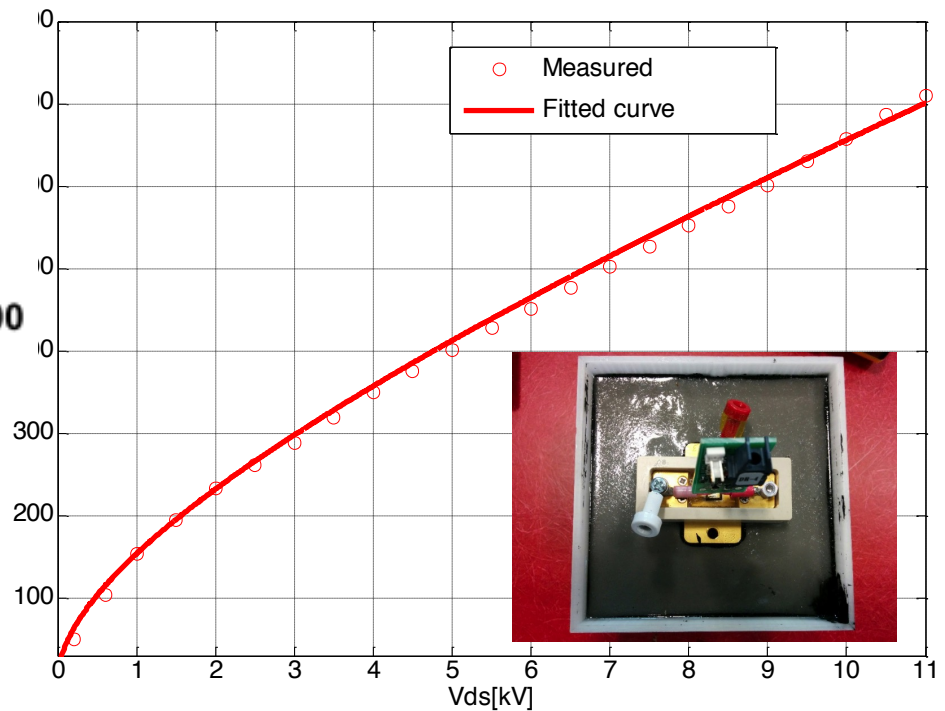


$$R_{on} = R_{on0} \left(\frac{T_j}{T_{j0}} \right)^{\alpha}$$

$$R_{on0} = 0.875 \Omega \quad T_{j0} = 348.16 \text{ K}$$

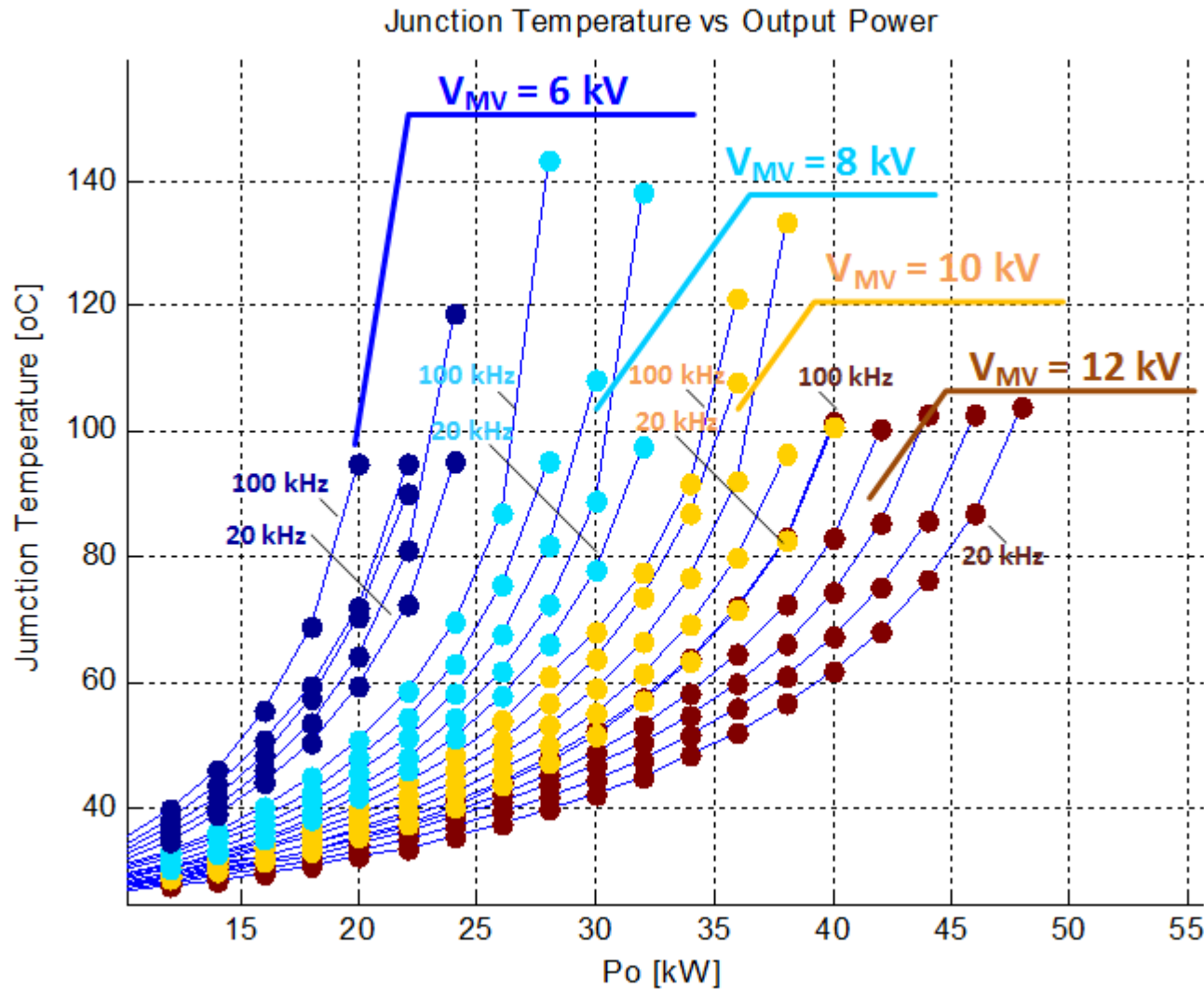
$$Q_{loss} = 4.08 \cdot 10^{-9} \sqrt{V_{ds}} + 24.8 \cdot 10^{-12} V_{ds}$$

Output Charge of 15kV SiC MOSFET & JBS



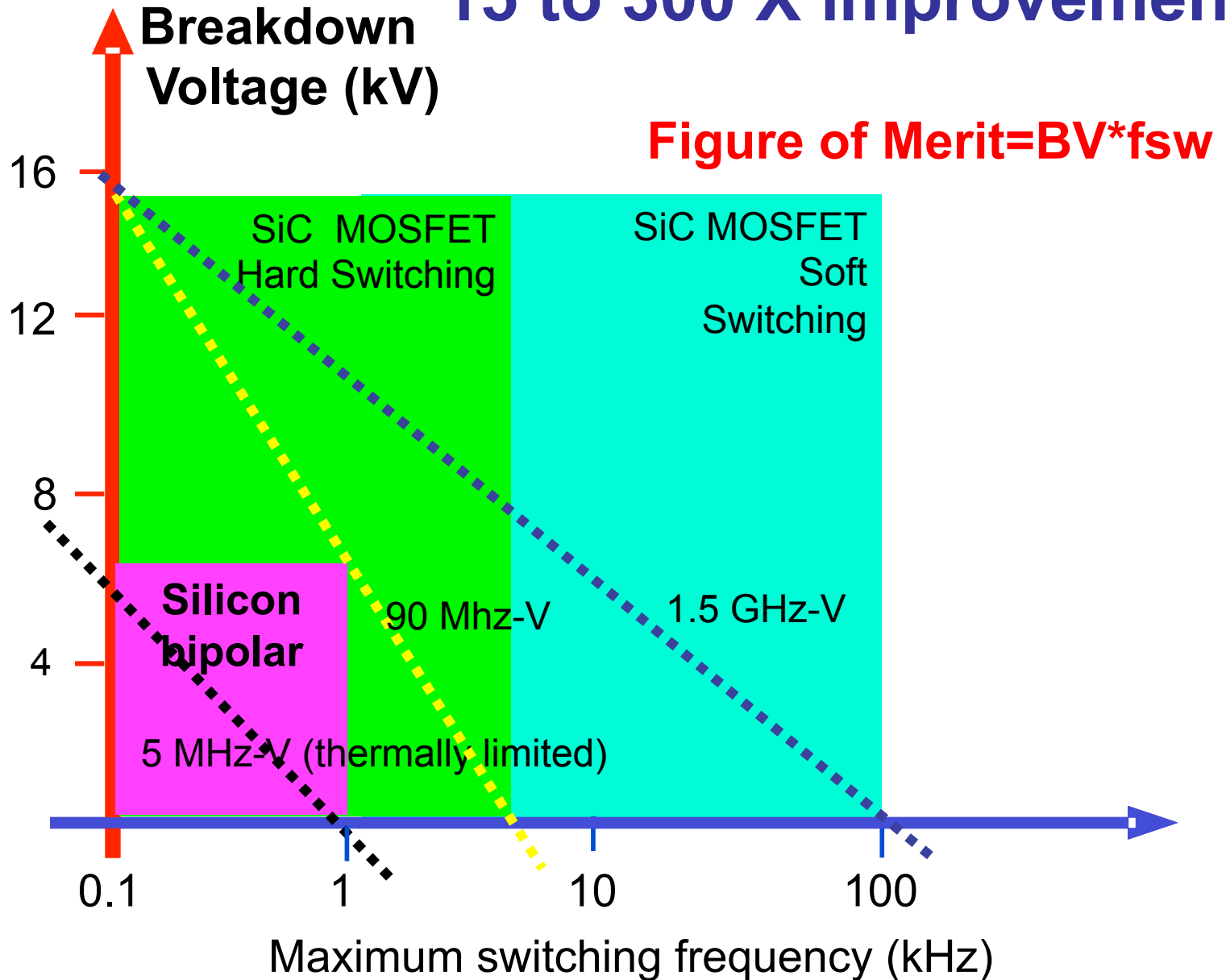
15 kV SiC MOSFET Capability: 100 kHz

Higher DC link voltage, Better device utilization →

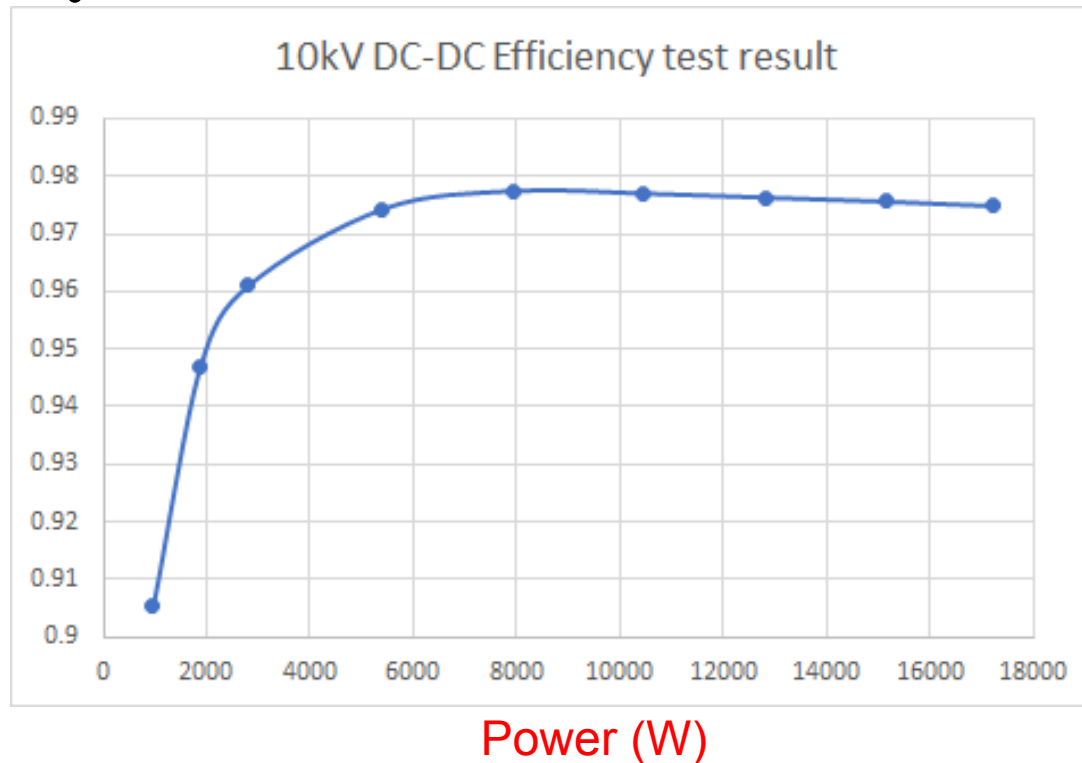
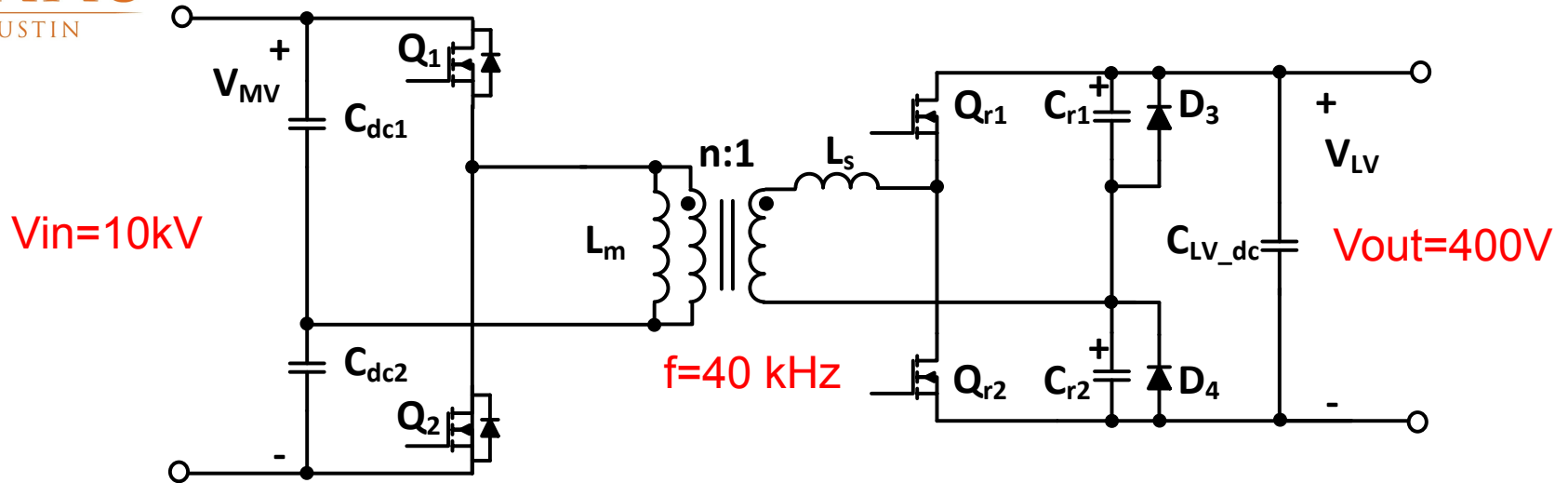


Only two 15 kV MOSFET used
Total SiC die size = 2 cm²

With SiC MOSFET: 15 to 300 X improvements

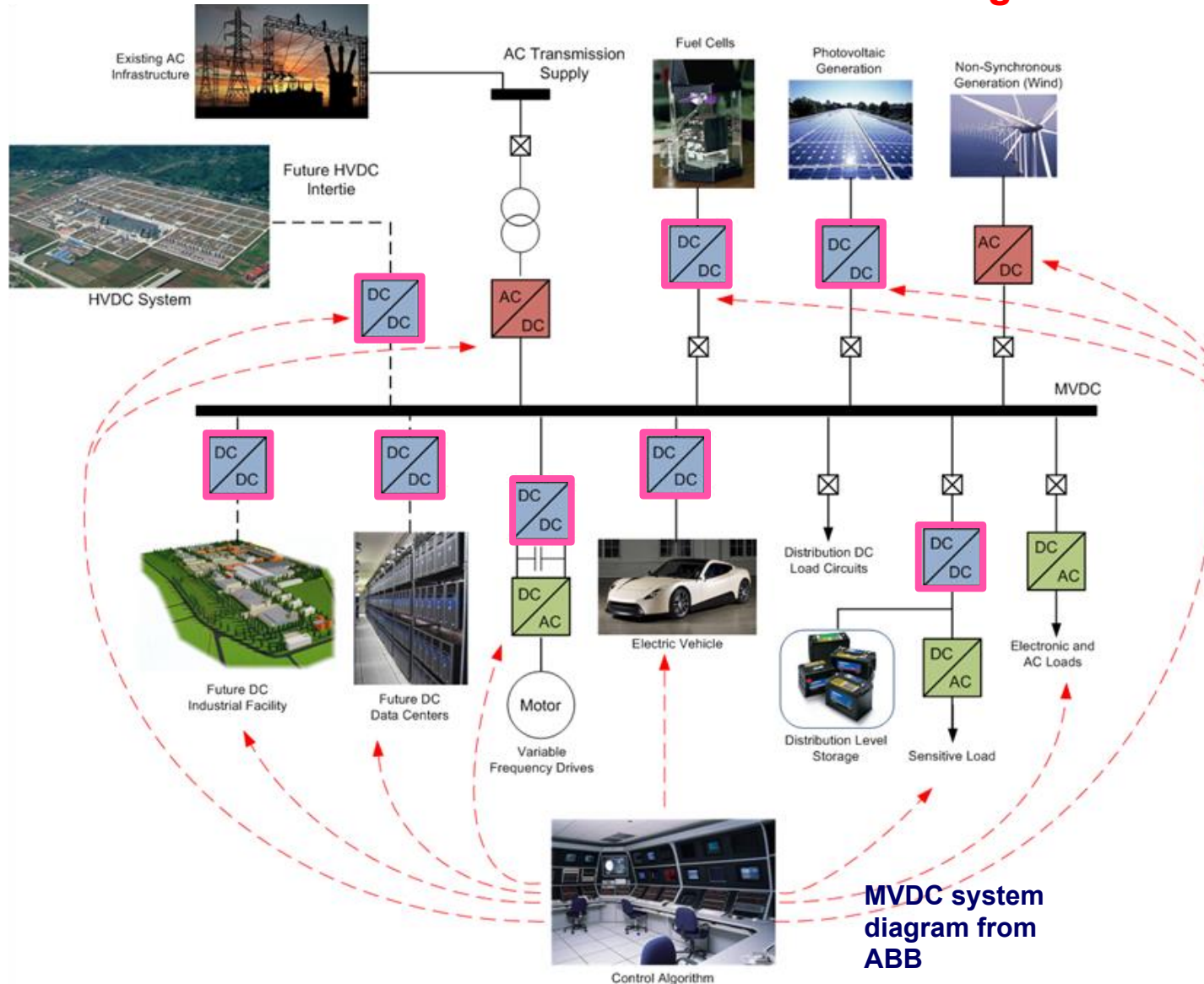


10 kV DCX: Two 15 kV SiC MOSFETs



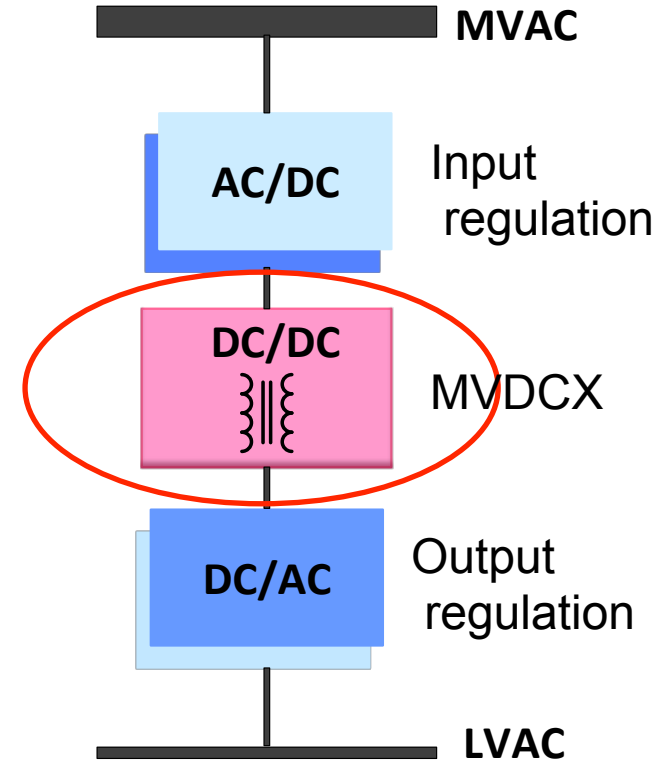
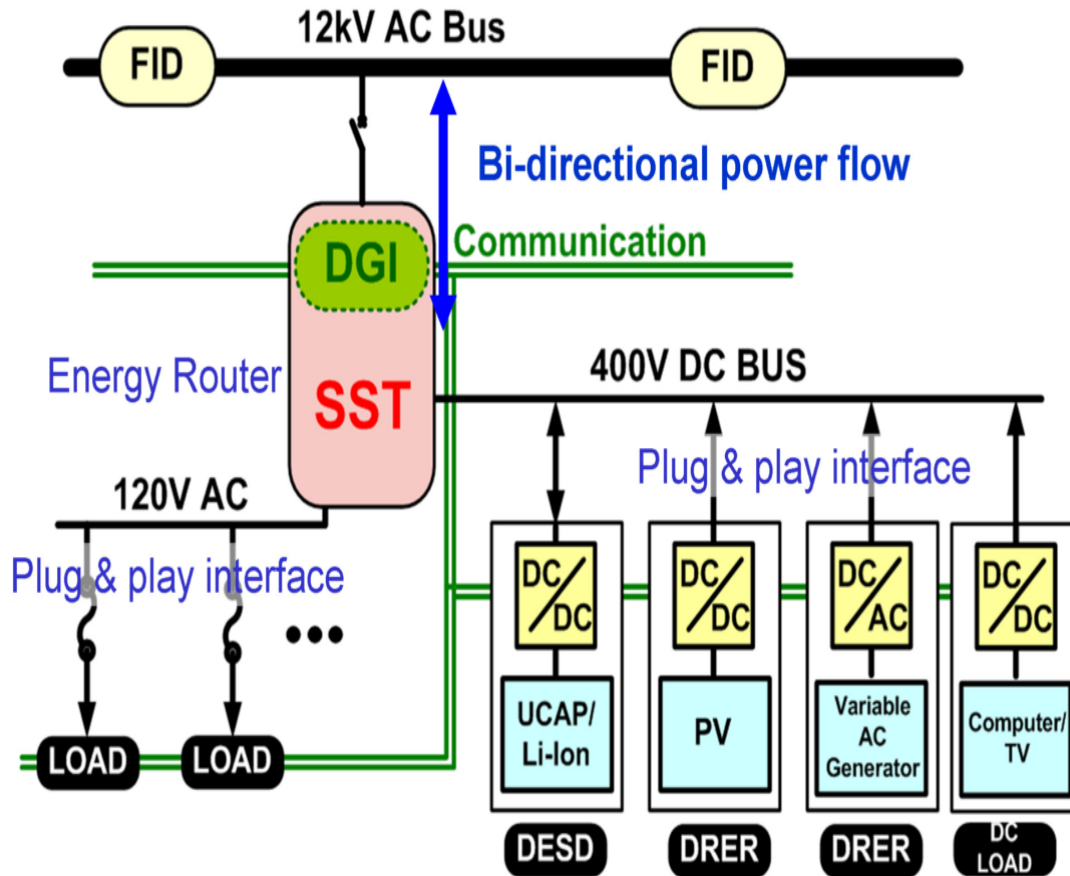
MVDC Application

MVDC Voltage: 10 to 20 kV



MVDC system diagram from ABB

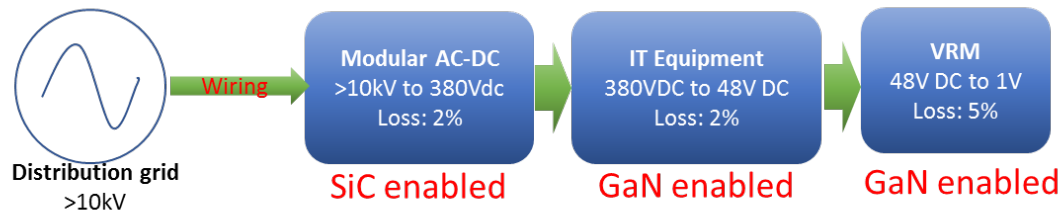
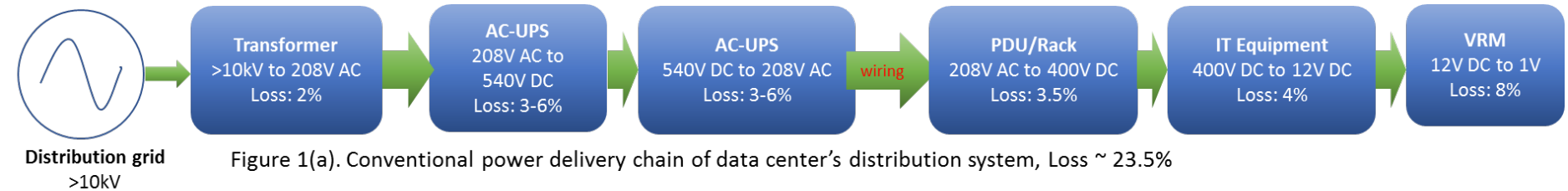
Solid State Transformer (Smart Transformer, Digital Transformer)



Role of Solid State Transformer (SST) in FREEDM Systems

Three Stage
SST

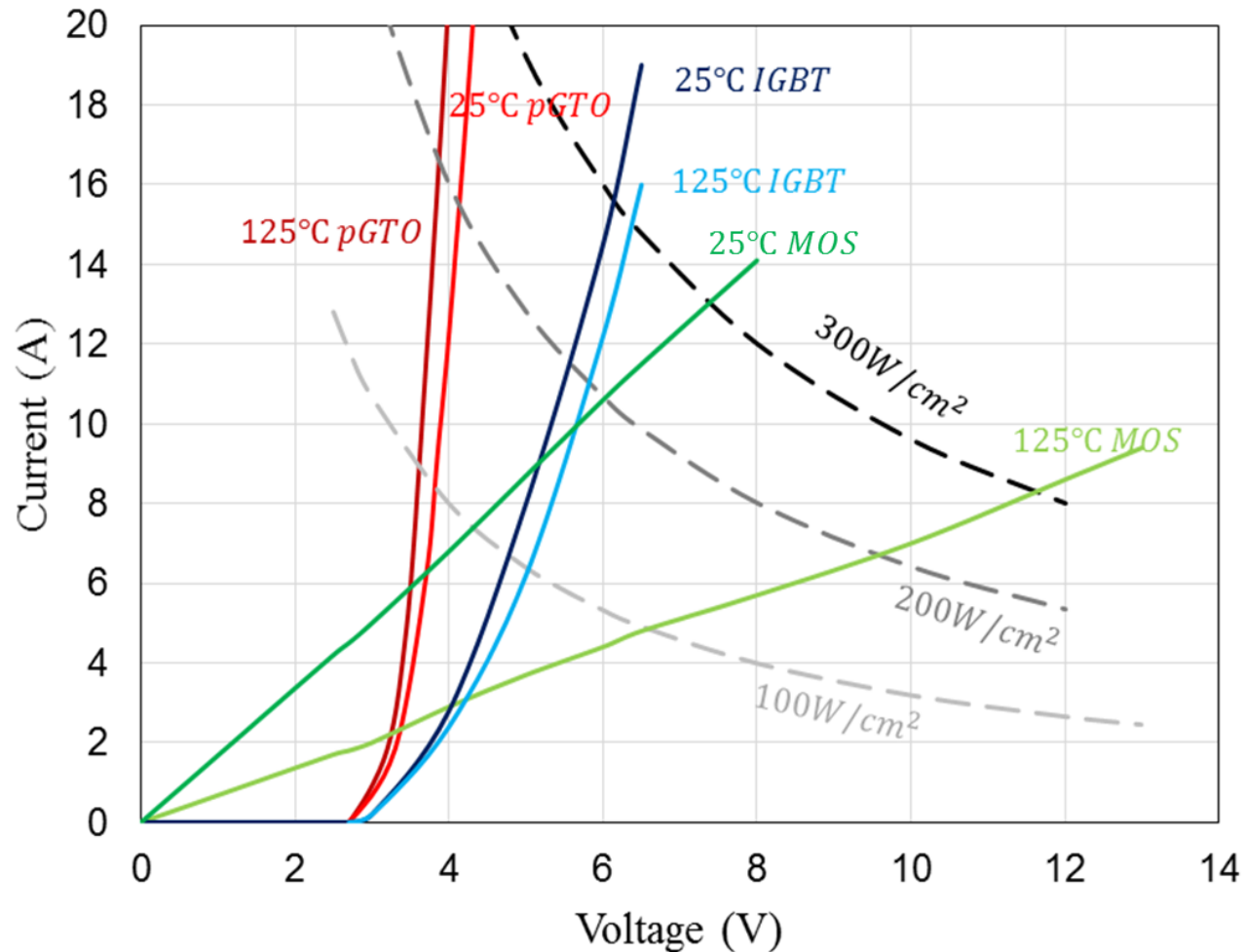
The impact we can make



14.5% loss reduction could mean 10 billion kWh of energy saving in US data center along

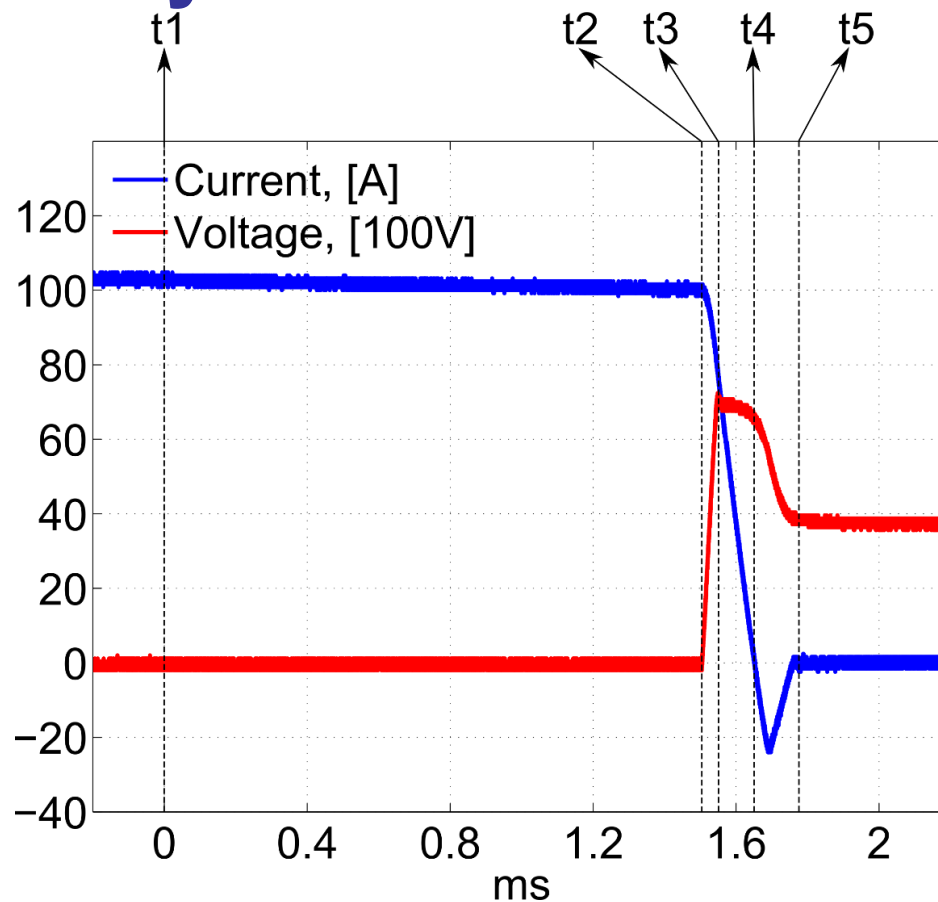
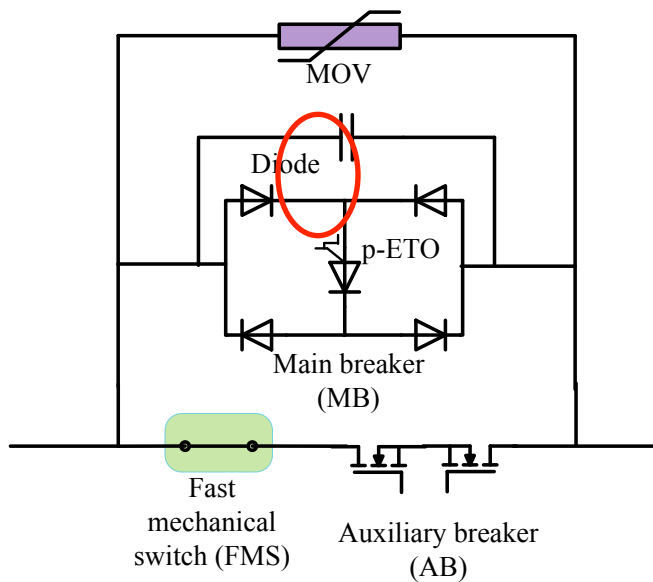
15kV SiC GTO, n-IGBT and MOSFET

$A=0.32\text{cm}^2$ or normalized to 0.32cm^2



SiC bipolar devices are more suitable for high power and high temperature operation

Solid state or hybrid DC circuit breaker



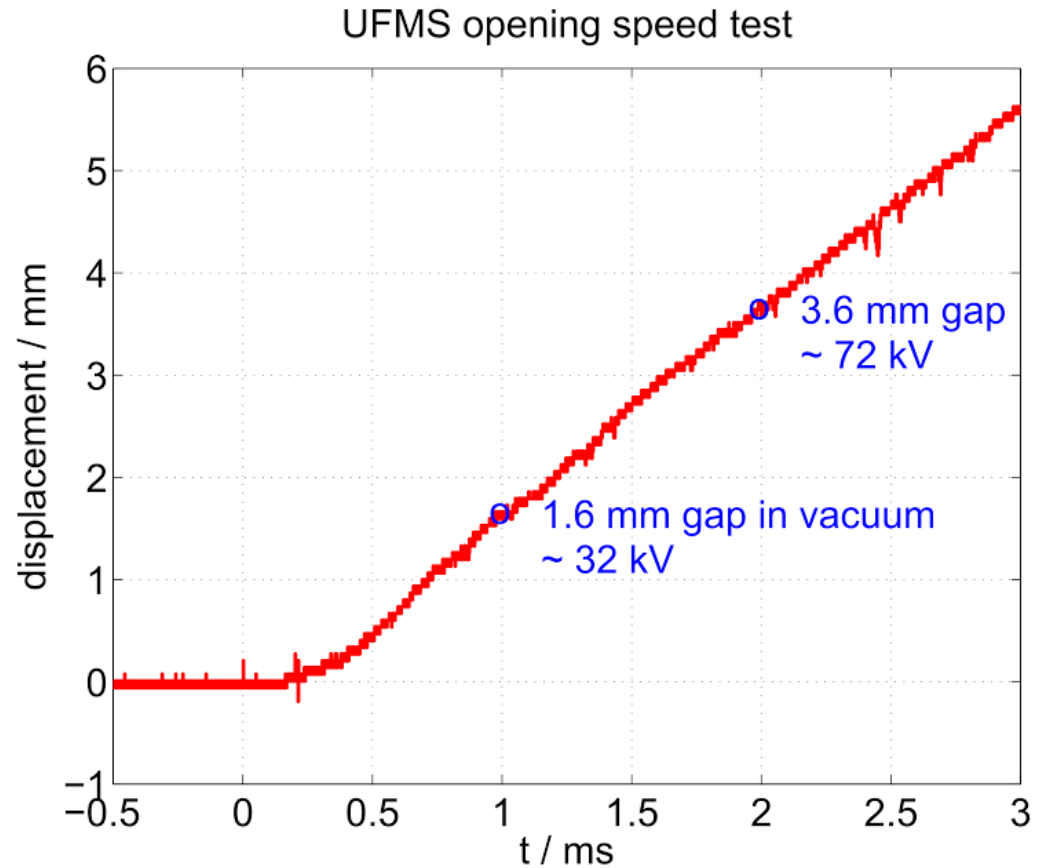
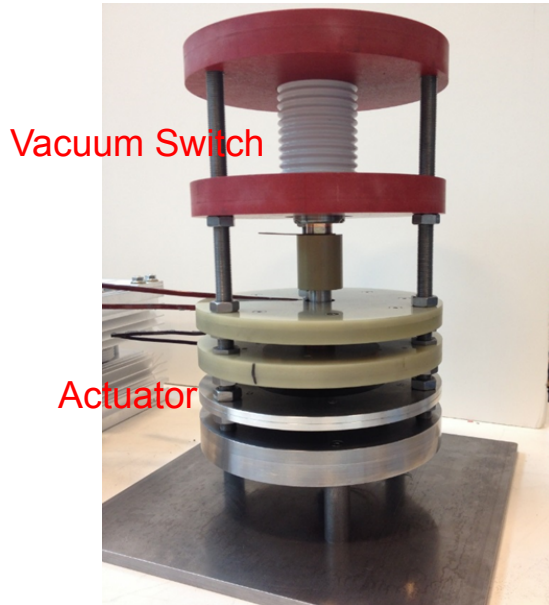
<2 ms interruption time

- $t_1 - t_2$: mechanical switch delay: 1.5 ms;
- $t_2 - t_3$: cap limited dv/dt ($100A/0.5 \mu F \sim 200V/\mu s$) rise b/c, $\sim 40 \mu s$;
- $t_3 - t_4$: MOV clamped at 7 kV, drives current to zero, $\sim 105 \mu s$;
- $t_4 - t_5$: diode reverse recovery and oscillation, $\sim 100 \mu s$.

FMS Based on Thomson Coil

1ms opening speed demonstrated and tested

15 kV/630A FMS
based on Thomson
coil actuator



Conclusions

WBG power devices scale the Voltage and Frequency capability well above and beyond Si capability

- **Frequency** scaling in LV power system will substantially improve the power density while maintaining high efficiency
- **Voltage*Frequency** scaling of SiC MOSFET can transformer the MV and HV power delivery system into a smart AC or DC power delivery system
- **Voltage** scaling of SiC Bipolar device can enable future generation of AC and DC circuit breakers

We look forward to the new partnerships